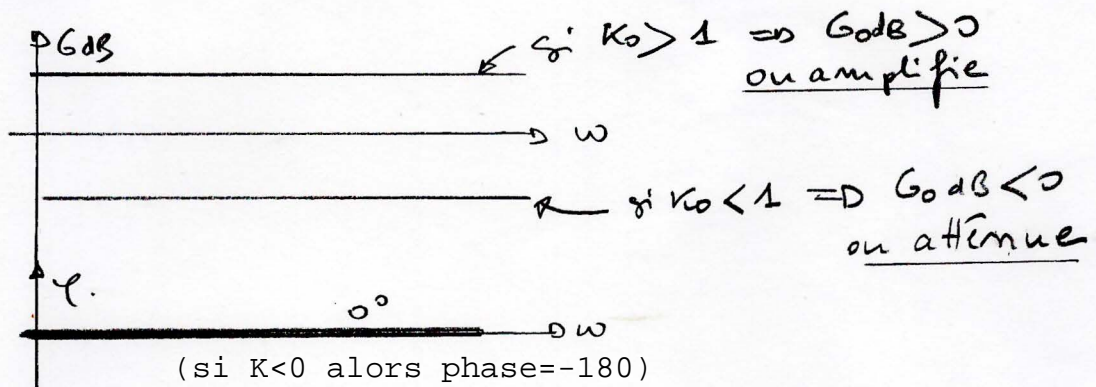


# Formes canoniques

- I - 1 -  $\text{Arg } H_0 = \text{Arg } K_0 = 0^\circ \rightarrow$  indépendant de  $\omega$ !  
 2 -  $|H_0| = K_0$  or  $G_{0dB} = 20 \log |K_0(j\omega)|$   
 $= 20 \log K_0 \rightarrow$  indépendant de  $\omega$ !

3. Allure Bode.



4 -  $\text{Arg } H_1(j\omega) = \text{Arg} \left( j \frac{\omega}{\omega_0} \right) = \frac{\pi}{2} \text{ rad.}$   
 $= 90^\circ$

5 -  $|H_1(j\omega)| = \left| j \frac{\omega}{\omega_0} \right| = \frac{\omega}{\omega_0} \Rightarrow G_{1dB} = 20 \log \left( \frac{\omega}{\omega_0} \right)$

6 - rappel  $\log \frac{a}{b} = \log a - \log b$   
 $\Rightarrow G_{1dB} = \underbrace{20 \log(\omega)}_a - \underbrace{20 \log \omega_0}_b$

7. représentation sous forme d'un Bode (semi-log)

axe x:  $\omega \mapsto l_\omega = k_x \times \log(\omega) + \frac{0}{2}$  si origine des  $\omega = 1$   
 $[cm] \quad [cm/déc]$

axe y:  $G_{1dB} \mapsto l_{G_1} = k_y \times G_{1dB} + 0$  si origine des dB  $\bar{\varnothing}$ .  
 $[cm] \quad [cm/dB]$

comme  $G_{1dB} = a \frac{\log \omega}{k_x} + b \Rightarrow l_{G_1} = a \frac{k_y}{k_x} l_\omega + k_y b$   
 $\frac{l_{G_1}}{k_y} \quad \frac{l_\omega}{k_x}$

équation d'une droite  
 part à l'origine  $a$   $b = -20 \log \omega_0$   
 $a = +20$   
 pente



Rq: prenons 1 exemple pour comprendre a

$$G(\omega = \omega_0) = a \log \omega_0 - a \log \omega_0 = 0 \text{ dB.}$$

(1 décade + loin

$$\begin{aligned} G(\omega = 10\omega_0) &= a \log(10\omega_0) - a \log \omega_0 \\ &= a \log 10 + a \log \omega_0 - a \log \omega_0 \\ &= a \log 10 = a = +20 \end{aligned}$$

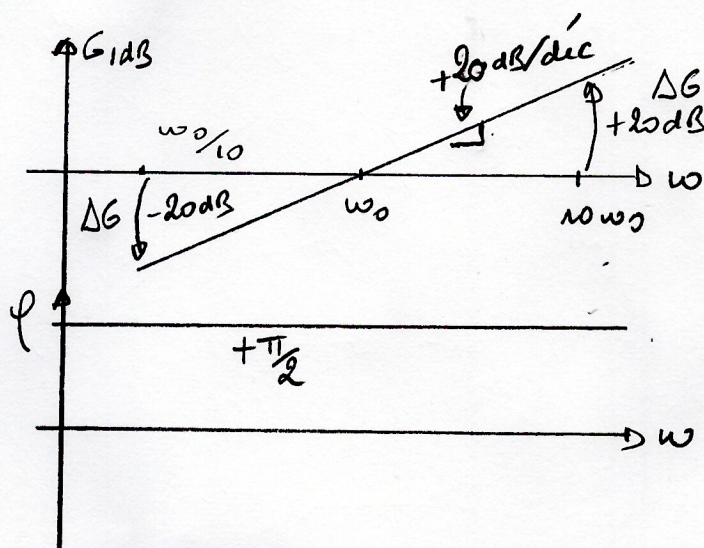
$$\Delta G = G(10\omega_0) - G(\omega_0) = +20 \text{ dB}$$

On dit que la pente est de  $+20 \text{ dB/décade}$ .

↳ par rapport à  $\omega_0$

- si  $\omega > \omega_0$  le signal est amplifié:  $G > 0$  et  $A > 1$ .
- si  $\omega < \omega_0$  le signal est atténué:  $G < 0$  et  $A < 1$

Allure du Bode



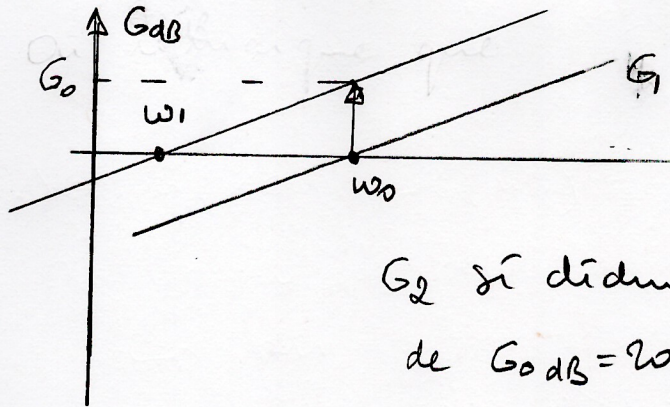


$$8. \quad H_2(j\omega) = K_0 j \frac{\omega}{\omega_0} = j \frac{\omega}{\frac{\omega_0}{K_0}} = j \frac{\omega}{\omega_1} \quad \text{avec } \omega_1 = \frac{\omega_0}{K_0}$$

$$G_2(\omega) = 20 \log \frac{\omega}{\frac{\omega_0}{K_0}}$$

$$\text{Pour } \omega = \omega_0 \quad G_2(\omega_0) = K_0$$

$$\omega = \omega_1 \quad G_2(\omega_1) = 0 \text{ dB.}$$



$G_2$  se déduit de  $G_1$  par translation.  
de  $G_{0dB} = 20 \log K_0$  (ici  $> 0$  pour l'exemple)

$$\text{Démonstration : } |H_2| = \left[ K_0 \times \frac{\omega}{\omega_0} \right] \\ = \left[ |H_0| \times |H_1| \right]$$

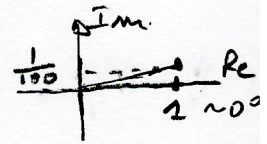
$$\Rightarrow \quad G_2 = 20 \log |H_2| = 20 \log |H_0| + 20 \log |H_1| \\ = 20 \log |H_0| + 20 \log |H_1| \\ = G_{0dB} + G_1dB$$



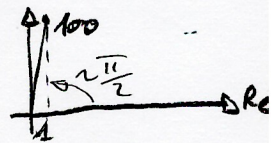
## formes canoniques : 1<sup>er</sup> ordre

$$1 - \text{Arg } H_3 = \varphi = \text{Arg} \left( 1 + j \frac{\omega}{\omega_3} \right) \\ = \text{Atan} \left( \frac{\omega}{\omega_3} \right) \quad \text{Rq: Atan ou } \tan^{-1} \text{ ou } \arctan$$

$$2 - \text{si } \omega \ll \omega_3 \Rightarrow \text{Arg } H_3 \rightarrow \text{Arg}(1 + j0) \\ \Rightarrow \varphi \rightarrow 0.$$

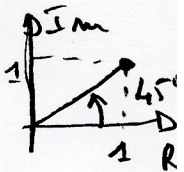


$$\text{si } \omega \gg \omega_3 \Rightarrow \text{Arg } H_3 \approx j \frac{\omega}{\omega_3} \text{ car } \left| \frac{\omega}{\omega_3} \right| \gg 1 \\ \varphi \rightarrow \frac{\pi}{2}$$



Rq: Point particulier (non demandé)

$$\text{si } \omega = \omega_3 \text{ alors } \text{Arg } H_3 = \text{Arg}(1 + j) \\ \varphi = 45^\circ = \frac{\pi}{4} \text{ rad.}$$



$$3 - |H_3(j\omega)| = \sqrt{1^2 + \left( \frac{\omega}{\omega_3} \right)^2}$$

$$G_{3dB} = 20 \log |H_3| = 20 \log \left[ 1^2 + \left( \frac{\omega}{\omega_3} \right)^2 \right]^{\frac{1}{2}} \\ = 10 \log \left[ 1^2 + \left( \frac{\omega}{\omega_3} \right)^2 \right]$$

$$4 - \text{si } \omega \ll \omega_3 \text{ alors } \left( \frac{\omega}{\omega_3} \right)^2 \ll 1^2$$

$$\Rightarrow |H_3| \sim 1 \Rightarrow G_{3dB} \rightarrow 0 \text{ dB}$$

$$\text{si } \omega \gg \omega_3 \text{ alors } \left( \frac{\omega}{\omega_3} \right)^2 \gg 1^2$$

$$|H_3| \sim \frac{\omega}{\omega_3} \Rightarrow G_{3dB} \sim 20 \log \frac{\omega}{\omega_3}$$

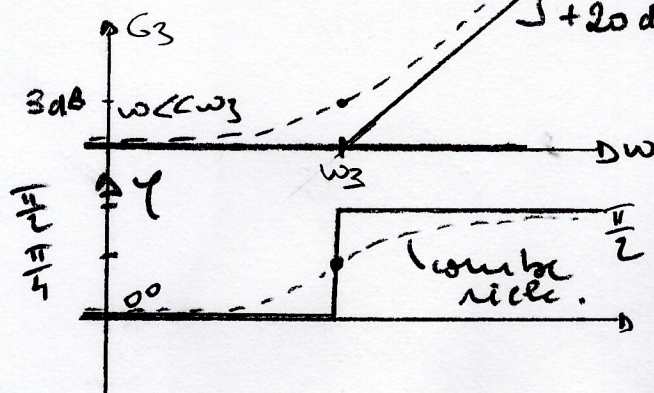
se comporte comme 1 dérivateur  
à haute fréquence

Rq: Point particulier:  $\omega = \omega_3$

$$\Rightarrow |H_3| = \sqrt{2} \text{ et } G_{3dB} = 20 \log \sqrt{2} = +3 \text{ dB}$$



5 - Bode de  $H_3$ .

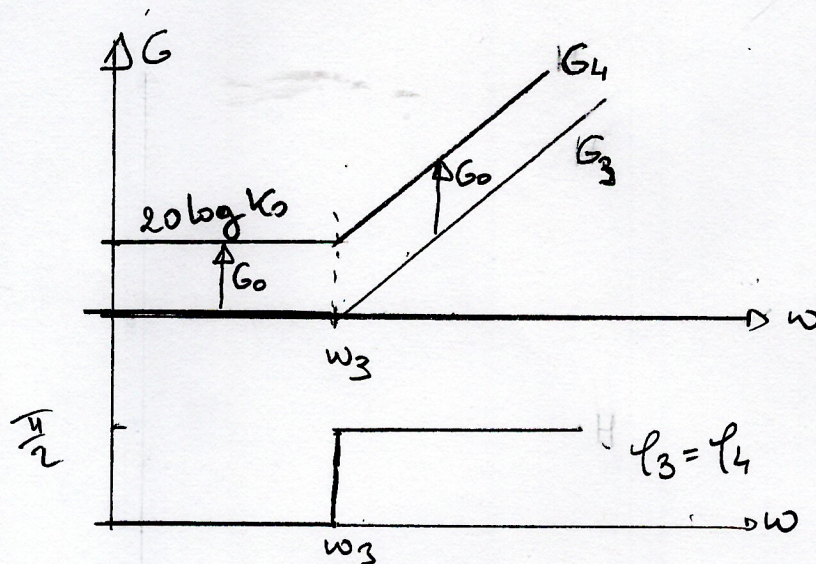


comportement global  
filtre passe haut  
(pseudo dérivateur)

$$6 - G_4 \text{ dB} = G_0 \text{ dB} + G_3 \text{ dB}$$

$$\text{Arg } H_4 = \text{Arg } H_0 + \text{Arg } H_3 = \text{Arg } H_3$$

$\varphi = 0^\circ$



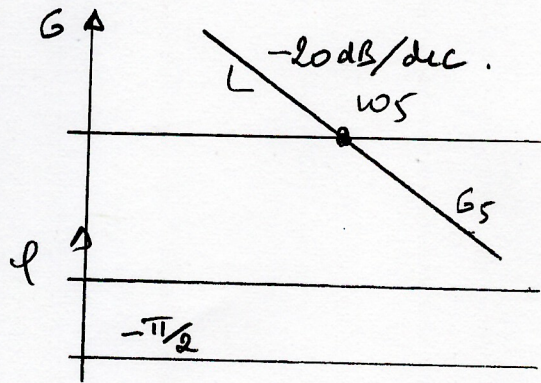


## IV Combinaisons.

•  $\underline{H_5} = \frac{K_5}{j\omega}$  = On cherche à mettre sous la forme  $\frac{1}{j\frac{\omega}{\omega_0}} = \frac{\omega_0}{j\omega} = \frac{1}{\underline{H_1}}$

$\underline{H_5} = K_5 \times \frac{\omega_0}{j\omega} = 1 = \frac{|K_5 \omega_0|}{j\omega} = \frac{\omega_5}{j\omega} = \frac{1}{j\frac{\omega}{\omega_5}}$  avec  $\omega_5 = \frac{1}{K_5}$  rad.

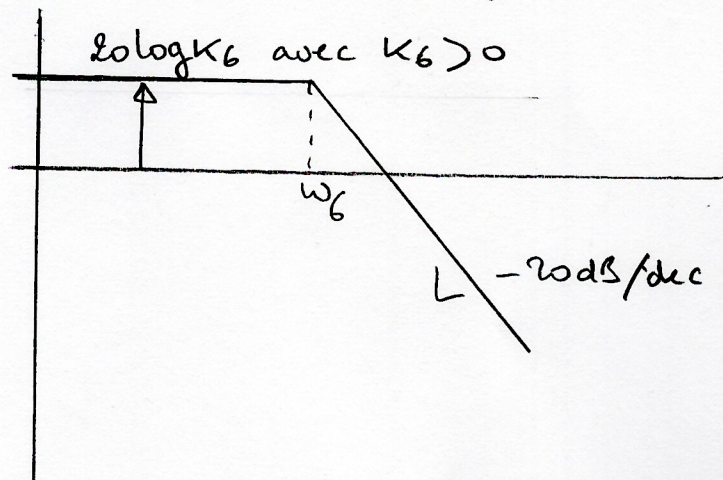
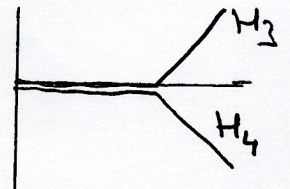
cl: forme "inverse" de  $\underline{H_2}$  (ou  $\underline{H_1}$ )



C'est un intégrateur pur.

•  $\underline{H_6} = \frac{K_6}{1 + j\frac{\omega}{\omega_6}} = \boxed{K_6} \times \boxed{\frac{1}{1 + j\frac{\omega}{\omega_6}}}$  - forme inverse de  $\underline{H_3}$ !

gain pur = décalage.

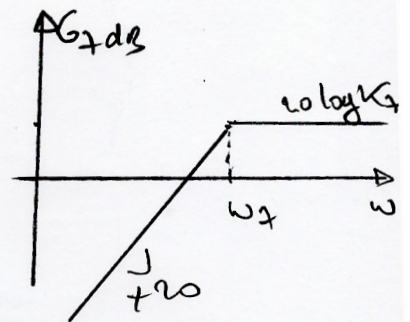
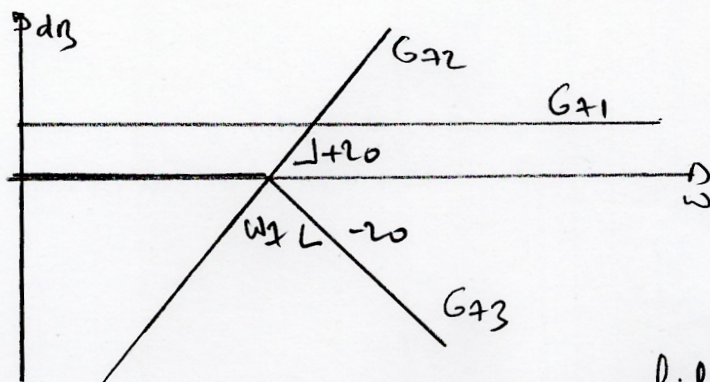


C'est un pseudo intégrateur (filtre passe BAS)



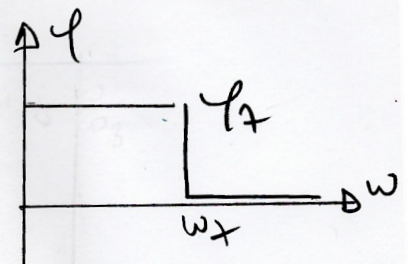
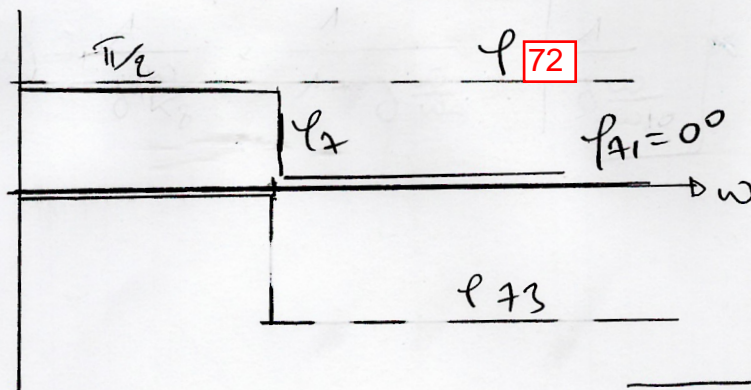
$$H_1(j\omega) = K_1 \times \frac{j\frac{\omega}{\omega_1}}{1 + j\frac{\omega}{\omega_1}} = \left[ K_1 \right] \times \left[ j\frac{\omega}{\omega_1} \right] \times \left[ \frac{1}{1 + j\frac{\omega}{\omega_1}} \right]$$

$$G_1 \text{ dB} = G_{11} + G_{12} + G_{13}$$



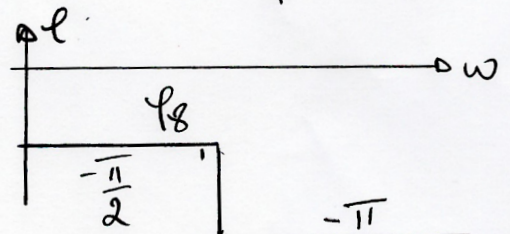
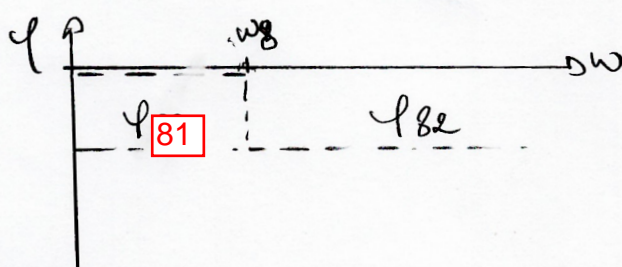
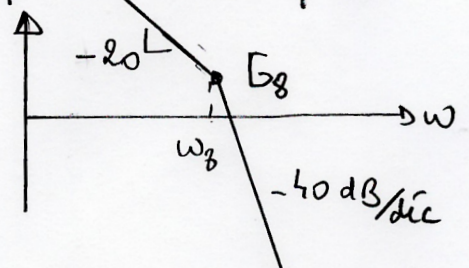
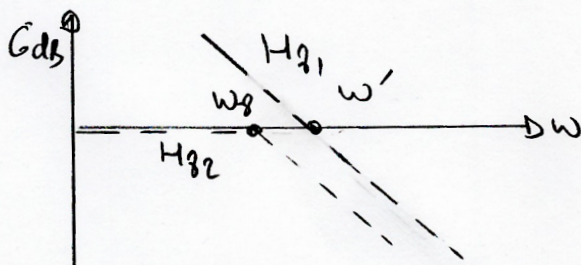
filtre passe haut  
(pseudo dérivateur)

$$\begin{aligned} \text{Ang } H_1 = & \text{Ang } H_{11} + \\ & \text{Ang } H_{12} + \\ & \text{Ang } H_{13} \end{aligned}$$



$$H_2(j\omega) = \frac{1}{j\frac{\omega}{\omega_2 \times 1}} \times \frac{1}{1 + j\frac{\omega}{\omega_2}} = \left[ \frac{1}{j\frac{\omega}{\omega_2}} \right] \times \left[ \frac{1}{1 + j\frac{\omega}{\omega_2}} \right]$$

formes canoniques

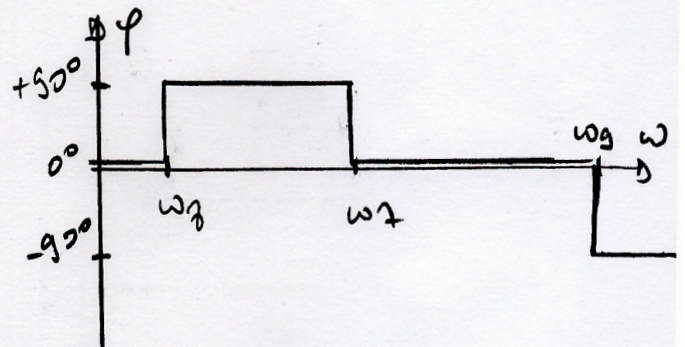
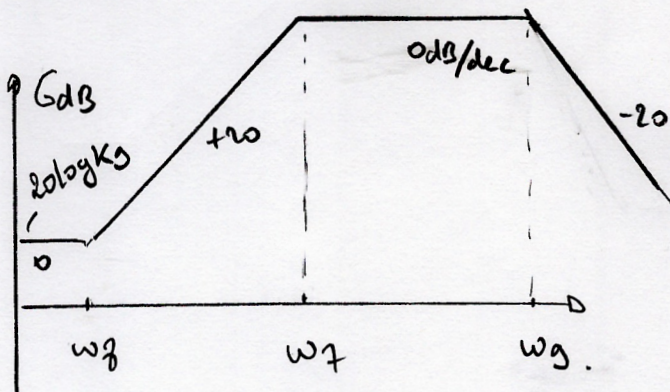
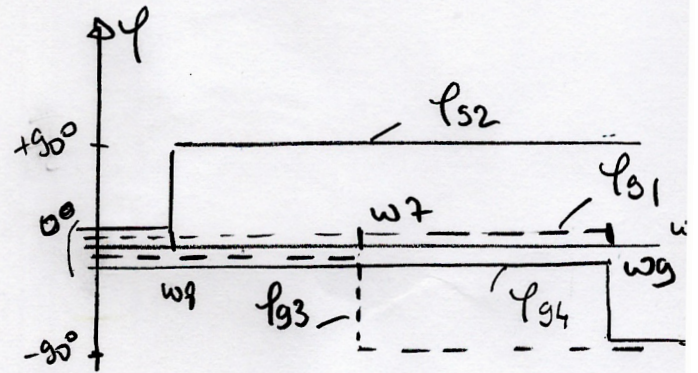
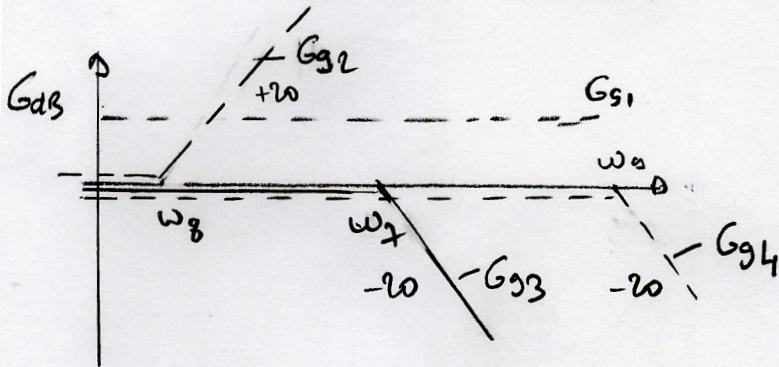




$$5 - H_g(j\omega) = \underbrace{K_g}_{H_{g1}} \times \underbrace{\left(1 + j\frac{\omega}{\omega_2}\right)}_{H_{g2}} \times \underbrace{\frac{1}{\left(1 + j\frac{\omega}{\omega_2}\right)}}_{H_{g3}} \times \underbrace{\frac{1}{\left(1 + j\frac{\omega}{\omega_3}\right)}}_{H_{g4}}$$

avec  $\omega_3 \ll \omega_2 \ll \omega_3$ .

( $R_g$ : l'ordre des pulsations de coupe influence le résultat !!)



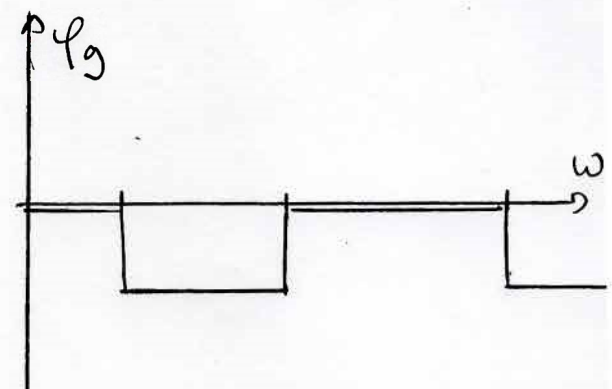
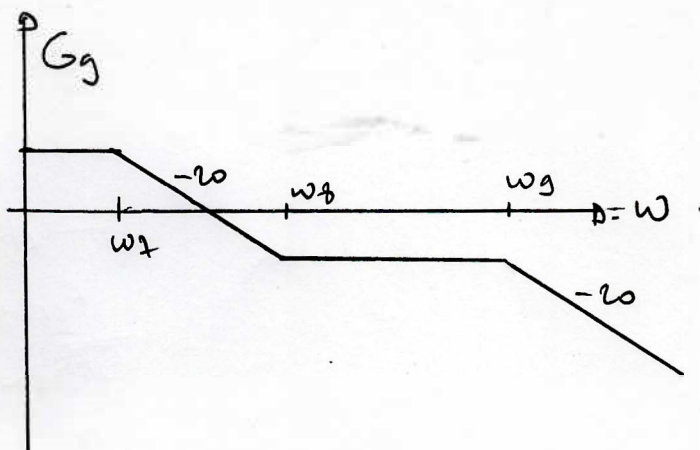
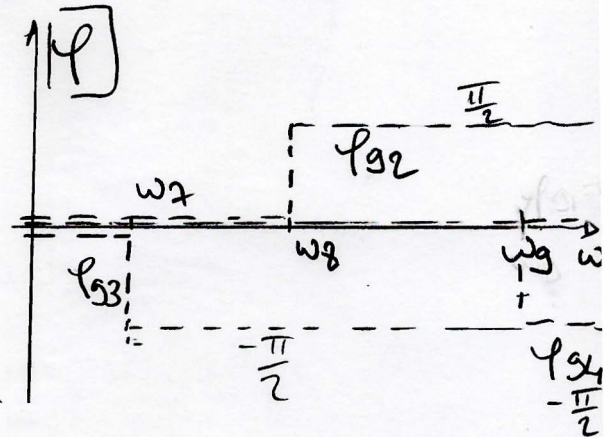
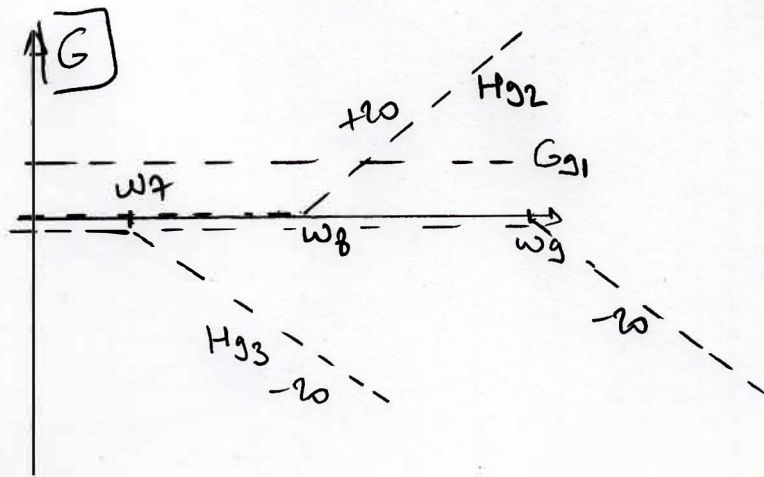
Bande passante

c'est 1 filtre  
passe bande



Bonus: etude lorsque  $w_7 \ll w_8 \ll w_9$

$$5 \quad H_g(j\omega) = \underbrace{K_g}_{H_{g1}} \times \underbrace{\left(1 + j\frac{\omega}{\omega_8}\right)}_{H_{g2}} \times \underbrace{\frac{1}{\left(1 + j\frac{\omega}{\omega_7}\right)}}_{H_{g3}} \times \underbrace{\frac{1}{\left(1 + j\frac{\omega}{\omega_9}\right)}}_{H_{g4}}$$



Rg : • Si  $\omega_7 \ll \omega_8 \ll \omega_9$  n'est pas vérifié  
alors il faut calculer  $G_g$  précisément.  
↳ Matlab, Matlab, Tableau